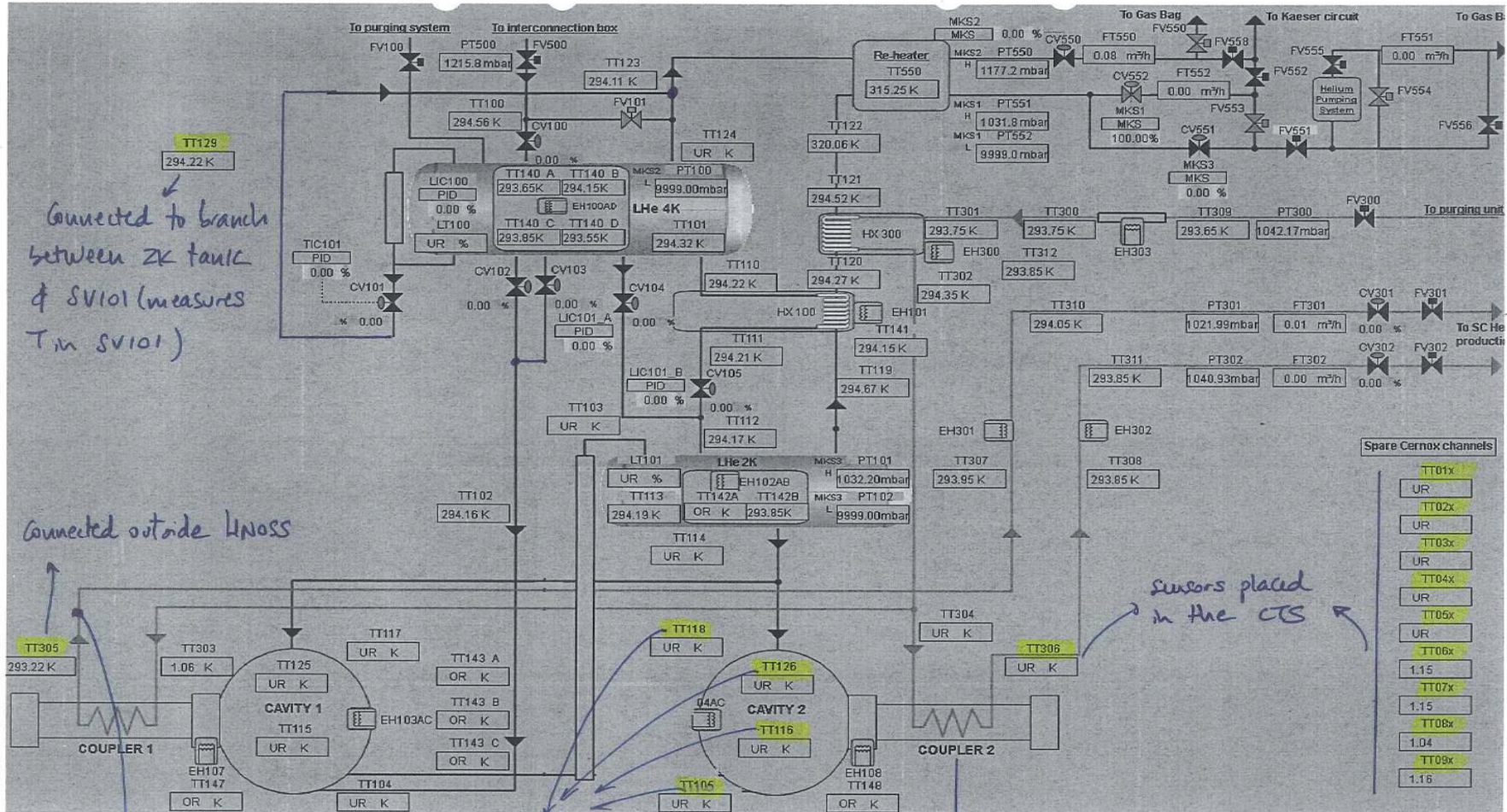




# Romea Tests (run #8)

## 23rd Feb-29th May

# Modifications



Connected to branch between 2K tank & SV101 (measures T<sub>in</sub> SV101)

Connected outside kross

this pipe is placed outside kross (port blinded inside kross)

Sensors used also for Cav 1 (placed in same positions as shown)

Copper plate with heater connected to EH (UX) in

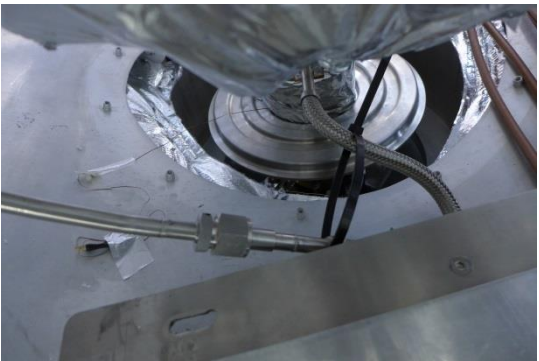
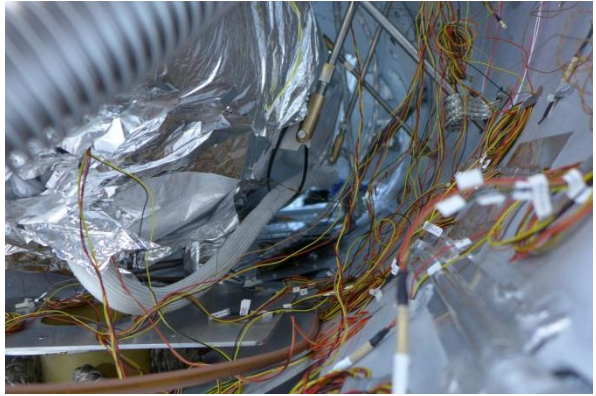
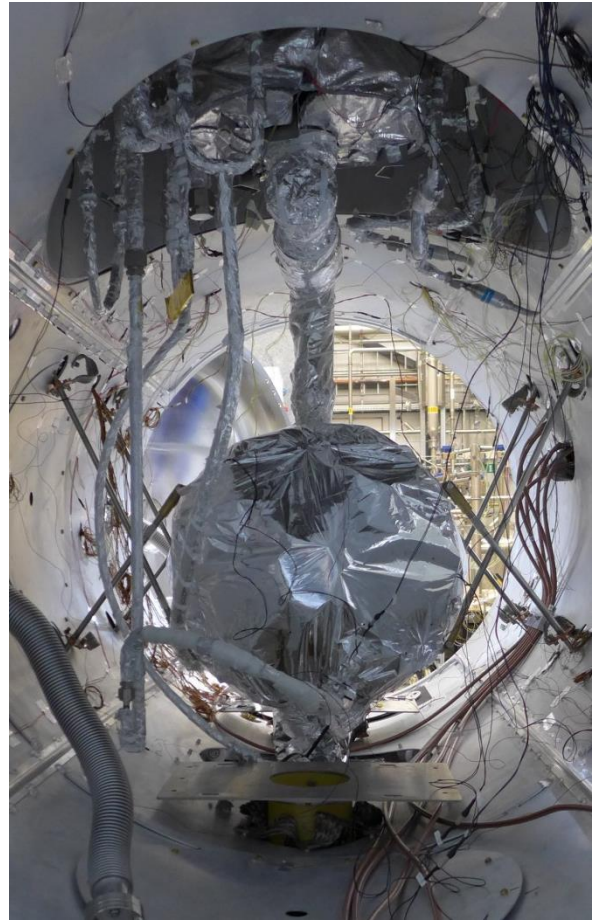
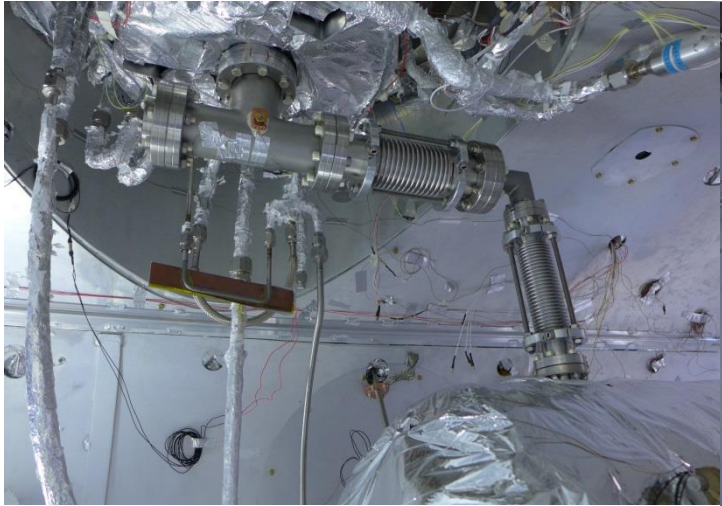
Sensors placed in the CTS

EUN #Y (Lower with FFC of CTS)

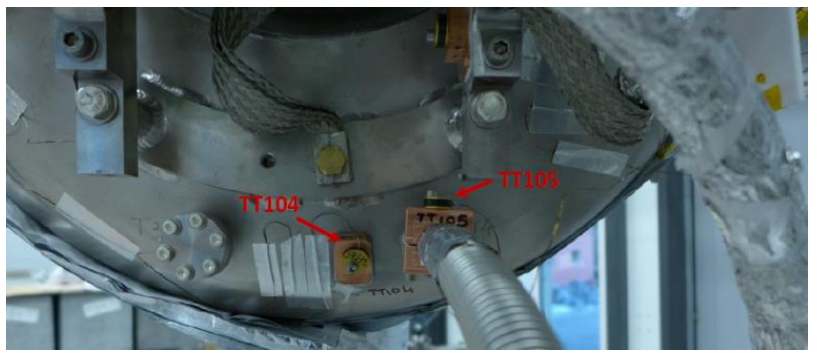
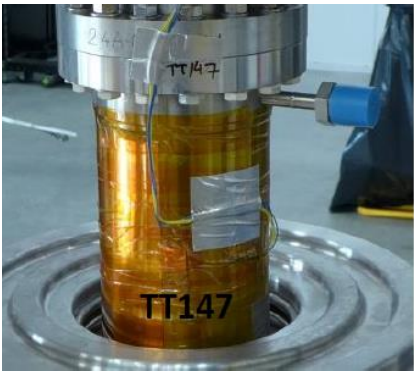
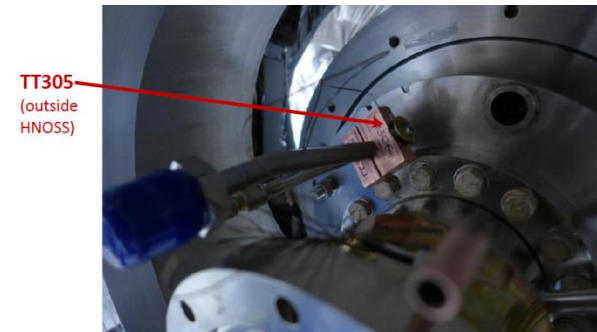
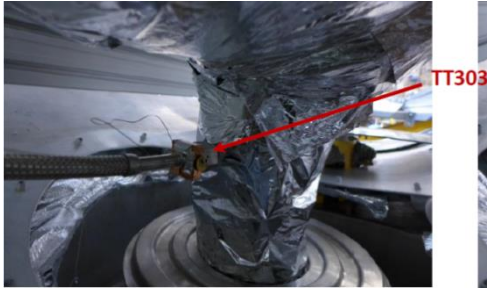
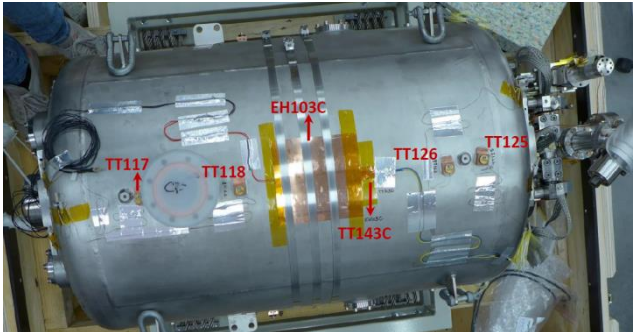
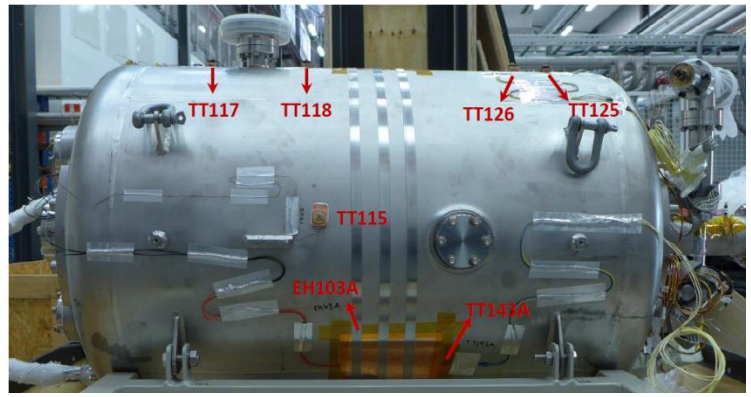
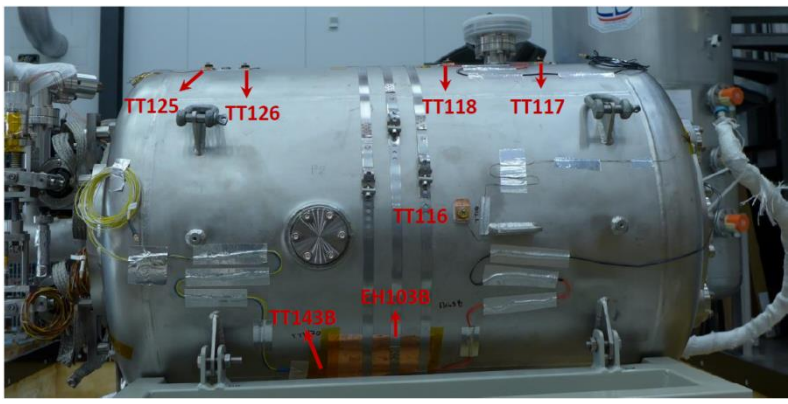
Spare Cernox channels

TT01x	UR
TT02x	UR
TT03x	UR
TT04x	UR
TT05x	UR
TT06x	1.15
TT07x	1.15
TT08x	1.04
TT09x	1.16

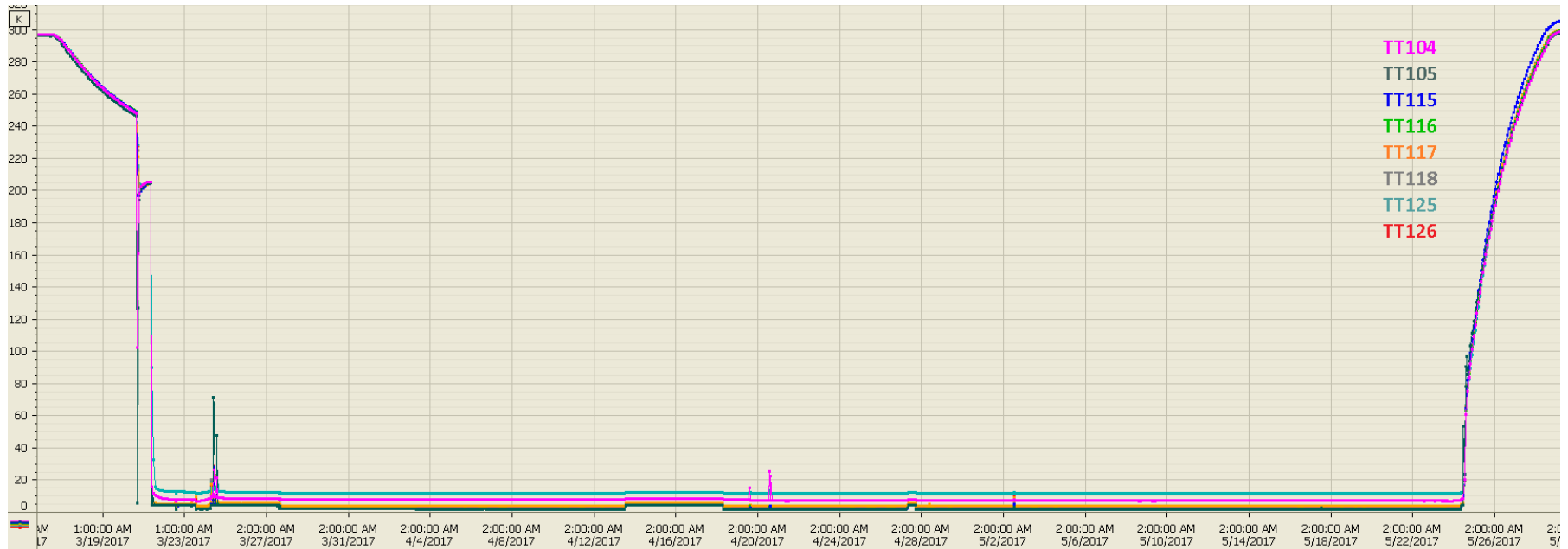
# Cryogenic setup



# Romea Sensors



During the whole run have kept Romea between 4K and 2K except for at the beginning, where the temperature was ca. 20 K for less than an hour.

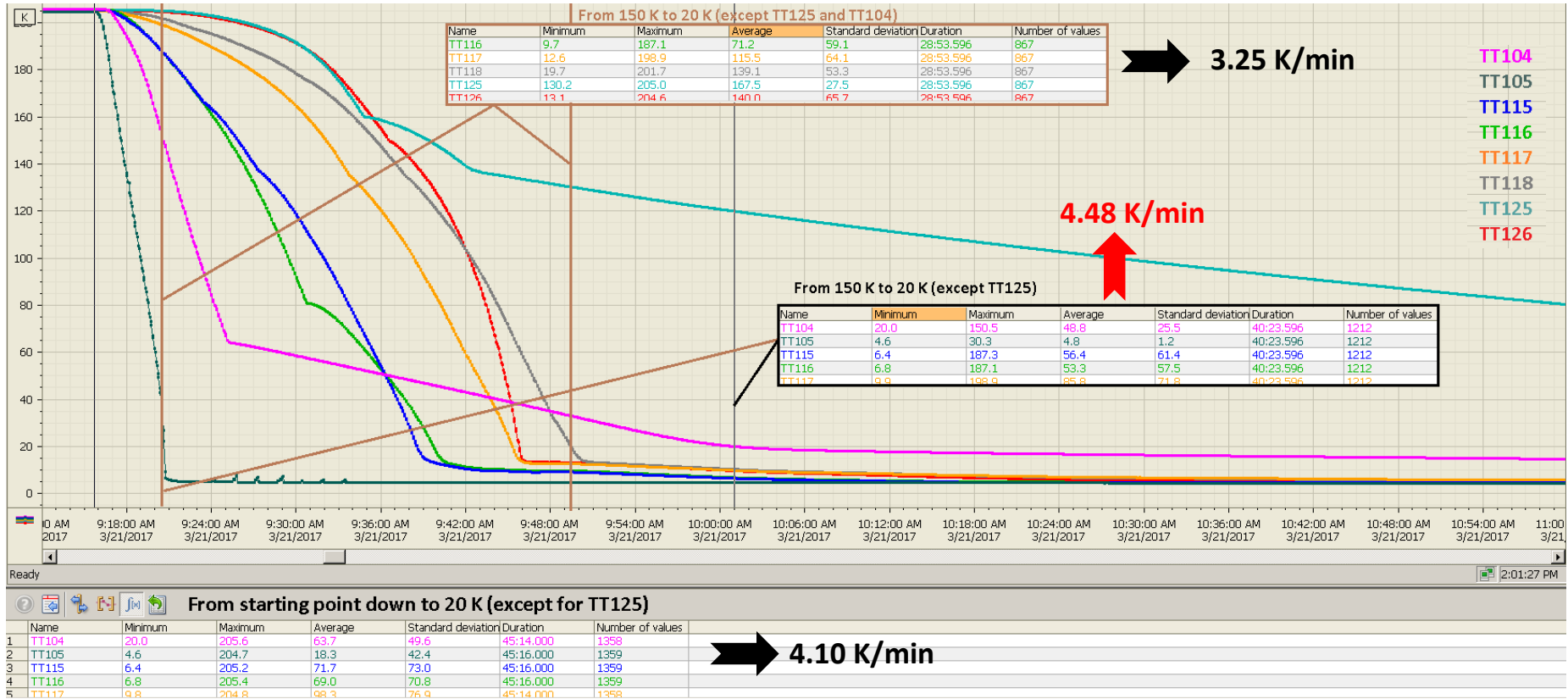


We saw that the insulation vacuum got spikes at the same time in both ICB and HNOSS, especially when intermitten filling.



On closer inspection it looks like the vacuum bursts in the ICB might be due to outgassing. For HNOSS is not that clear since the vacuum "ondulates" when in regulation mode, so we might have a leak in the 2K circuit (graph shown when at 20 mbar)



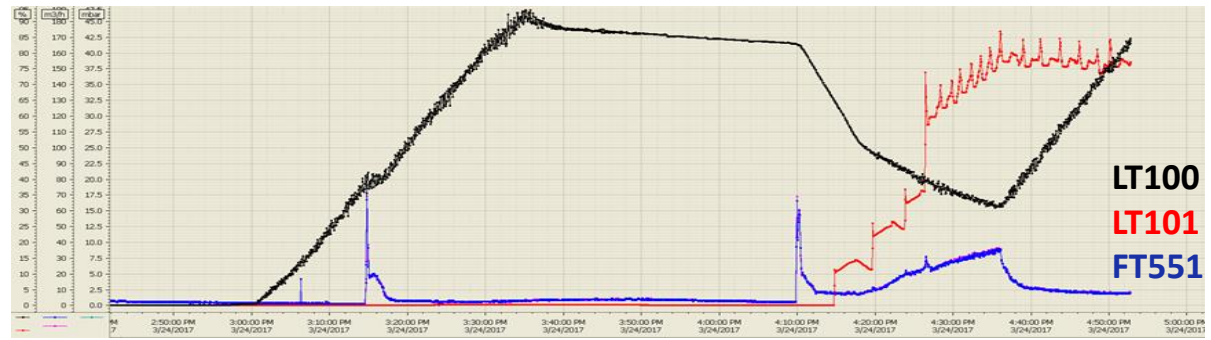


After tests saw that TT104 had come off. Still have not visually checked TT125 but expect a similar outcome.

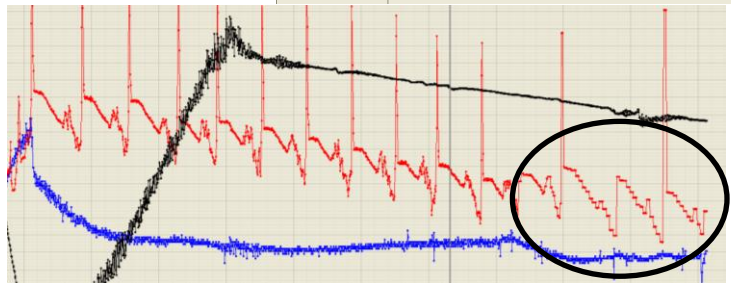
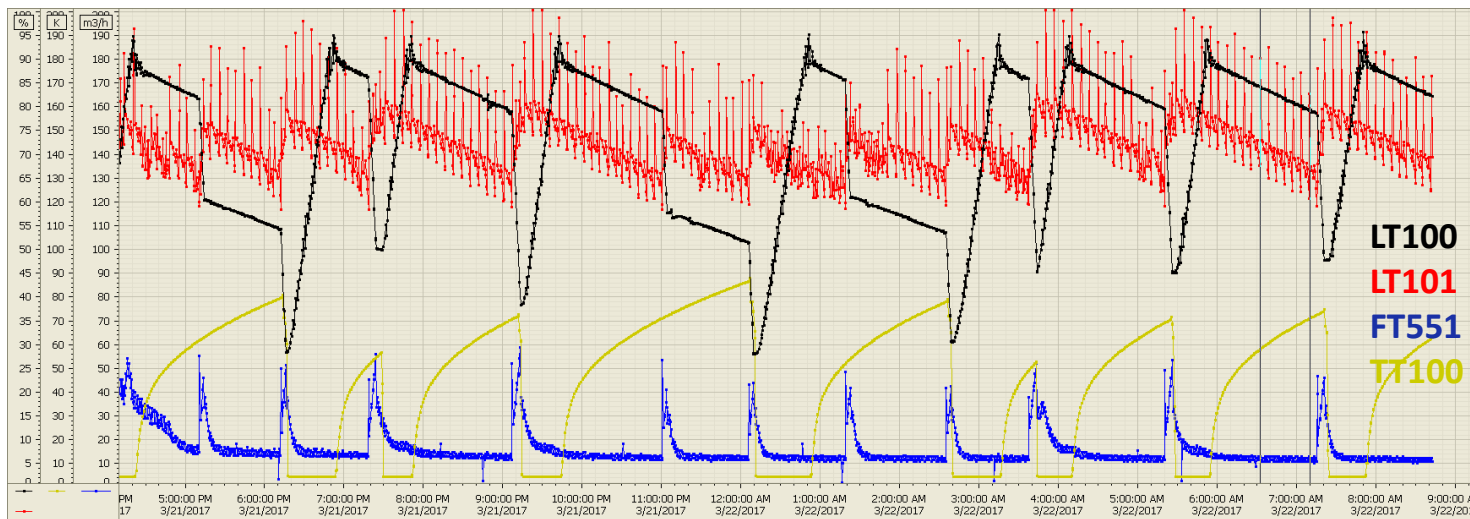
# LT101 Spikes (1/2)



1000 mbar, start cooldown of cavity, get spikes in FT551



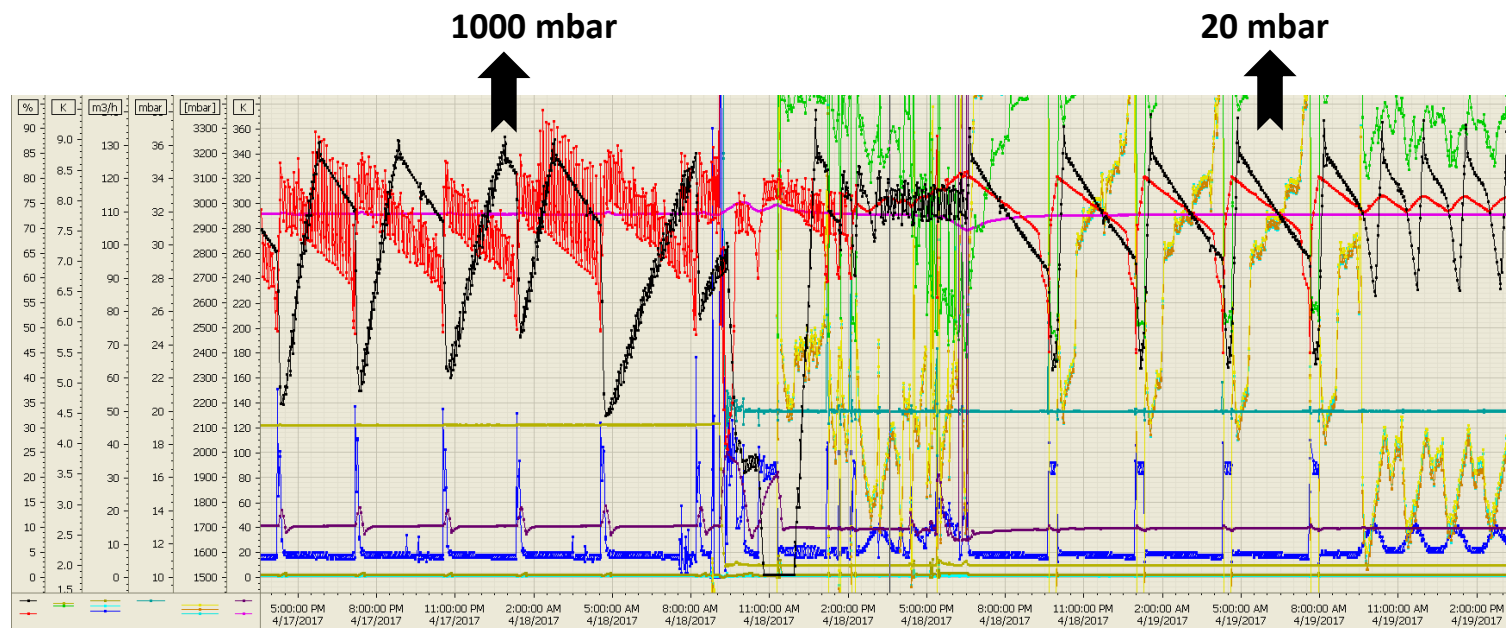
1000 mbar, no RF or heating power, no FT551 spikes, cavity cold for some days already (spikes are ca. 6 min apart)



Reduced the sampling in the AMI controller → did not work, still got spikes

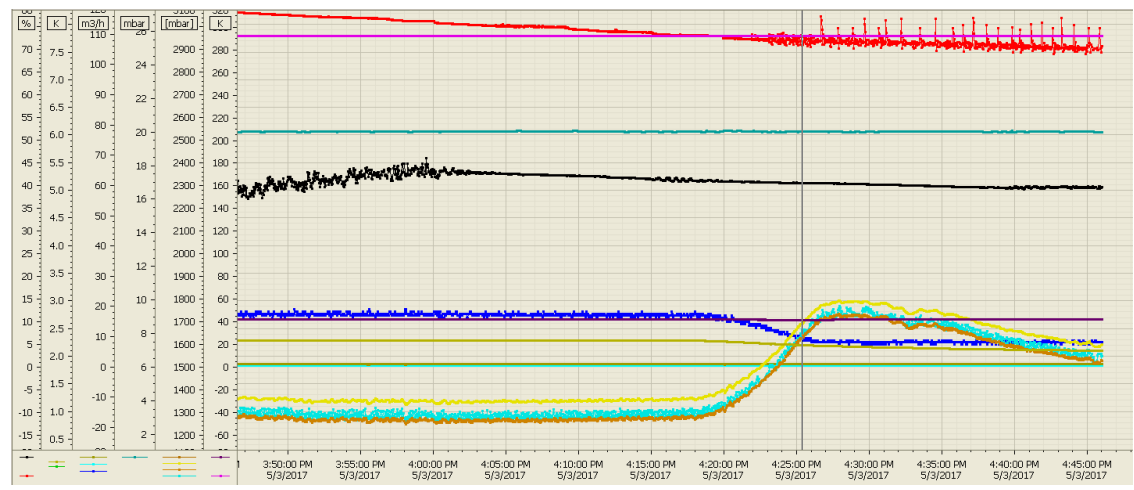


# LT101 Spikes (2/2)



LT100  
LT101  
FT551

A couple of times we have got spikes after switching off power (here applied 12W in heat)

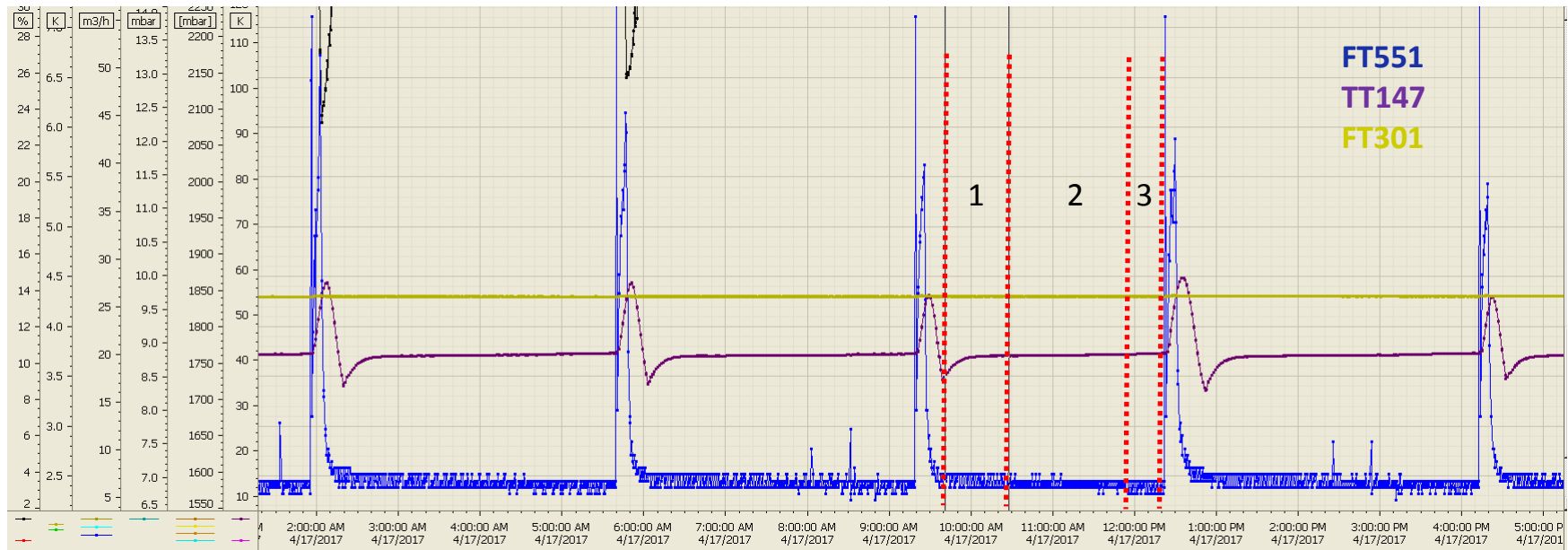


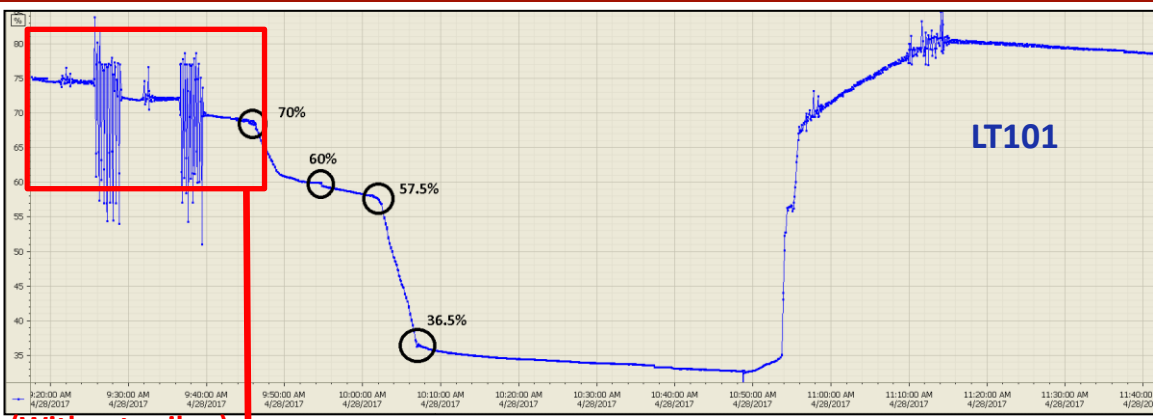
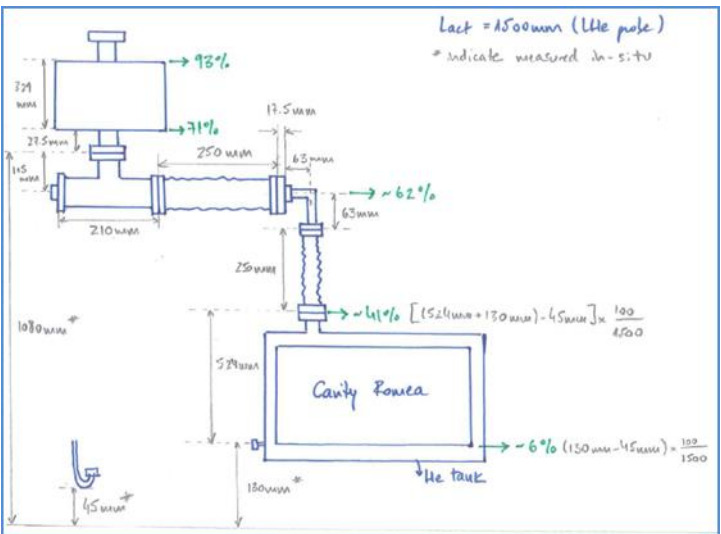
- Because of the spikes, not easy to measure
- Roughly identified three (3) regions
- Note: CV104 was closed and no RF /heat power was applied during measurements

FT551 [m3/h]	Std dev [m3/h]	LT101 Region
6.7	0.3	
6.4	0.3	2
6.2	0.3	3

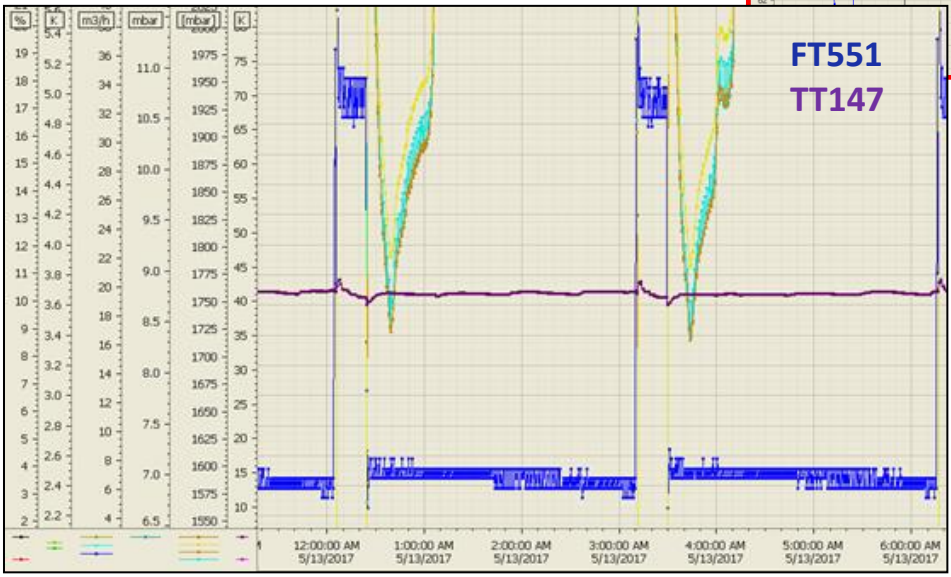
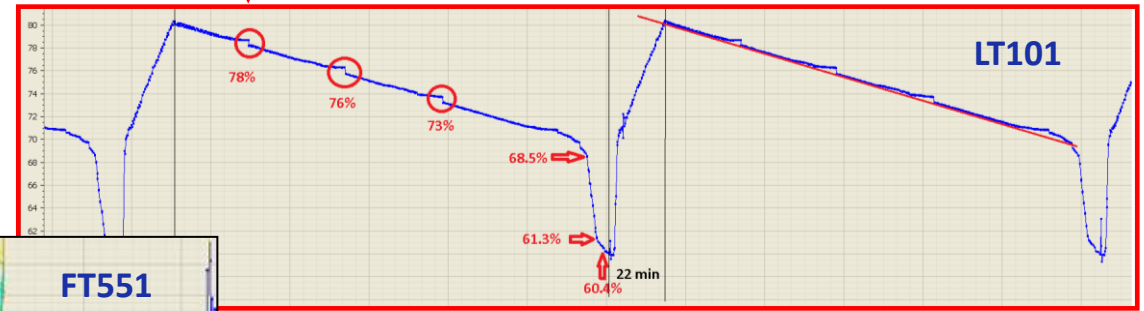


Average static heat loads at 4K are 6.5 m3/h





(Without spikes)



Identified four (4) regions with no filling (CV105 off)

FT551 [m3/h]	Std dev [m3/h]	LT101	
		min [%]	max [%]
7.12	0.34	76	80
6.81	0.31	72	76
6.54	0.33	69	72
6.11	0.33	60	69

At 20 mbar, measured the effect of CV105 on FT551 when varying opening of CV105

Note:

- The 4K tank was at ca. 1.2 bar
- The temperature of the coupler TT147 was kept at a constant temperature
- There was no RF/heat power applied during the experiments

CV105	TT147		FT551	
	[%]	[K]	[m3/h]	std dev
5	42.2	0	8.5	0.3
10	42.1	0	9.4	0.4
15	42.2	0	10.8	0.4
20	42	0.1	12.6	0.4
30	41.8	0	16.2	0.5
50	41.8	0	22.3	0.5
100	41.6	0.3	32.5	0.8

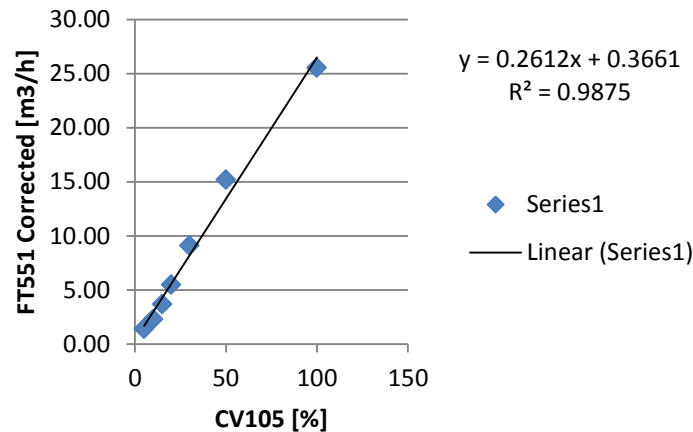
Measurement

LT101	LT101 correction
[%]	[m3/h]
78-80	7.12
78	7.12
78	7.12
78	7.12
79	7.12
79-80	7.12
73-80	$(7.12+6.81)/2=6.96$

Correction depending on level

FT551 corrected	
[m3/h]	% from total
1.38	<b>16.27</b>
2.28	<b>24.29</b>
3.68	<b>34.10</b>
5.48	<b>43.52</b>
9.08	<b>56.07</b>
15.18	<b>68.09</b>
25.54	<b>78.58</b>

Flow from CV105 only



At 20 mbar, measured the effect of TT147 on FT551 when varying opening of FT301

Note:

- CV105 was kept closed
- There was no RF/heat power applied during the experiments

TT147		FT551	
[K]	std dev	[m3/h]	std dev
42.4	0.1	6.5	0.3
81-91.5		7.07	0.34
85-90		8.3	0.4
32.1	0	7.2	0.3
31.9	0.1	6.9	0.3

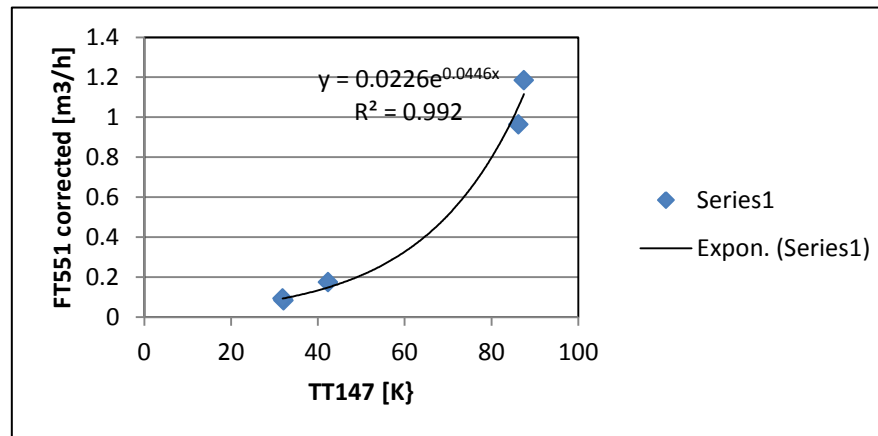
Measurement

LT101	LT101 correction
[%]	[m3/h]
68-72	(6.81+6.54)/2
67.5-68	6.11
79-80	7.12
76-77	7.12
73-74.6	6.81

Correction depending on level

FT551 corrected
[m3/h]
0.175
0.96
1.18
0.08
0.09

Effect of TT147



From this experiment we concluded that the effect of TT147 on FT551 is minimal below 90K (less than max 1W).

At 20 mbar, measured the effect of heat power on FT551 when connecting EH103AB to an external power supply and vary the voltage.

Note:

- The correction for the voltage at the heater side was found to be 0.942
- CV105 was kept closed
- TT147 was kept well below 90K

EH103		FT551	
[W]	[m3/h]	std dev	
2	8.2	0.3	
4	10.8	0.4	
8	13.8	0.4	
10	14.7	0.5	
12	17.3	0.5	
12	17.5	0.5	
12	17.3	0.5	

Measurement



EH103 correction		FT551	
[W = m3/h]	[m3/h]	std dev	
1.88	8.2	0.3	
3.77	10.8	0.4	
7.54	13.8	0.4	
9.42	14.7	0.5	
11.30	17.3	0.5	
11.30	17.5	0.5	
11.30	17.3	0.5	

Correction depending on power



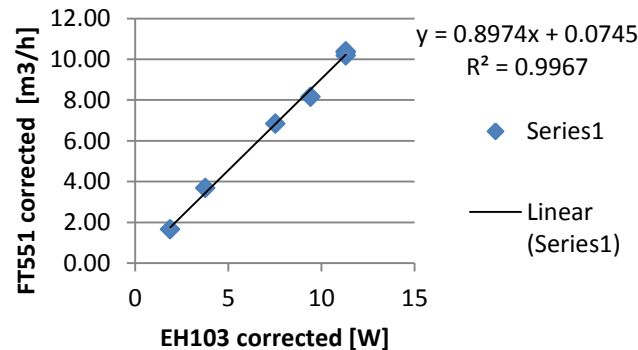
LT101		LT101 correction	
[%]	[m3/h]		
70-72	6.54		
79-80	7.12		
75-77	(7.12+6.81)/2=6.96		
70-72	6.54		
77-80	7.12		
76-79	7.12		
74-80	(7.12+6.81)/2=6.96		

Level correction




FT551 corrected	
[W = m3/h]	
1.66	
3.68	
6.84	
8.16	
10.18	
10.38	
10.34	

Power dissipated by the cavity



- Note:
  - TT304 and TT306 (for coupler 2) were not in place
  - All RF measurements have been done with CV105 closed
  - IPNO set at inlet temperature of and outlet of 300K and with a flow of 46 mg/s

## RF power couplers 1/4



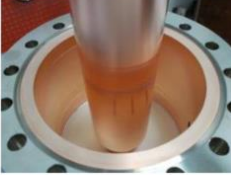


Electromagnetic RF wave

Coupler	
Single ceramic window	
TiN coating (nm)	~ 5 – 10
Frequency [MHz]	352.21
P max [kW]	400

⇒ 4 prototypes manufactured (PMB; CST)

• Inner conductor (antenna)

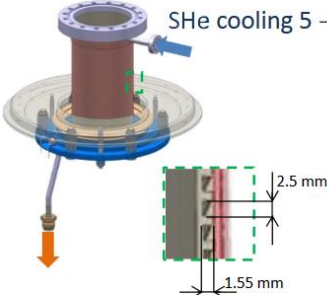
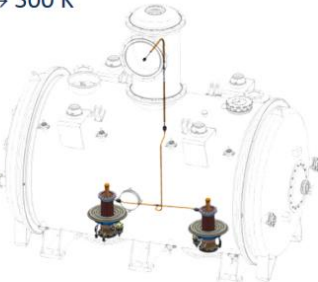




Inner water cooling circuit

RF power coupler (1 ceramic window)

MUSICC 3D soft. ⇒ multipacting simulations

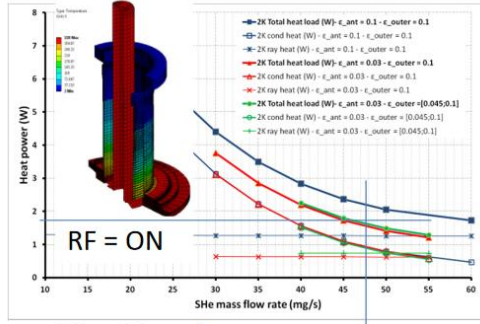
• Outer conductor (antenna)

She cooling 5 → 300 K

2.5 mm

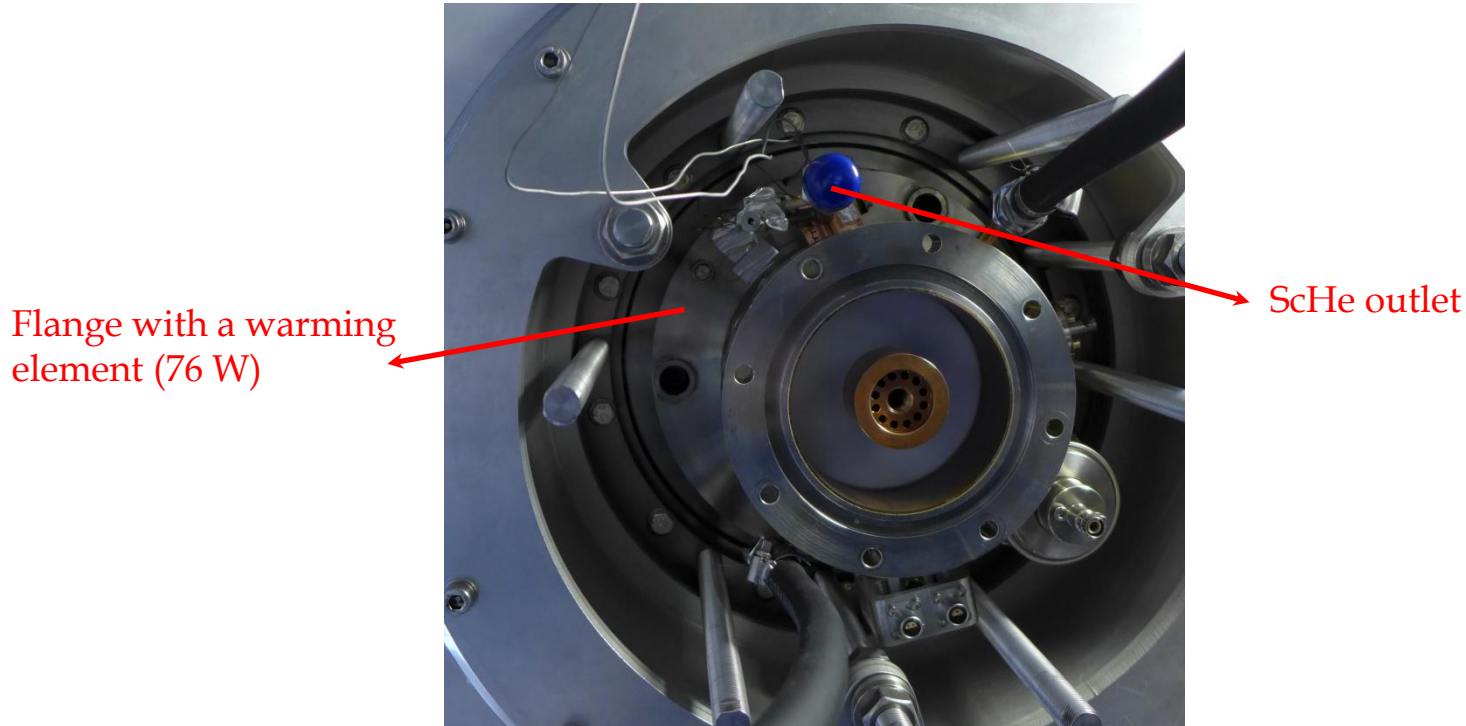
1.55 mm



RF = ON

⇒ SHE: 46 mg/s

- First, we tried temperature regulation for only Coupler 1 and set it to 9K, but TT305 was at 266K despite the FPC having a heater on the last flange before the ScHe is sent out (76 W in power). Had to add an extra heater band and wrap it around the line to avoid it from freezing.

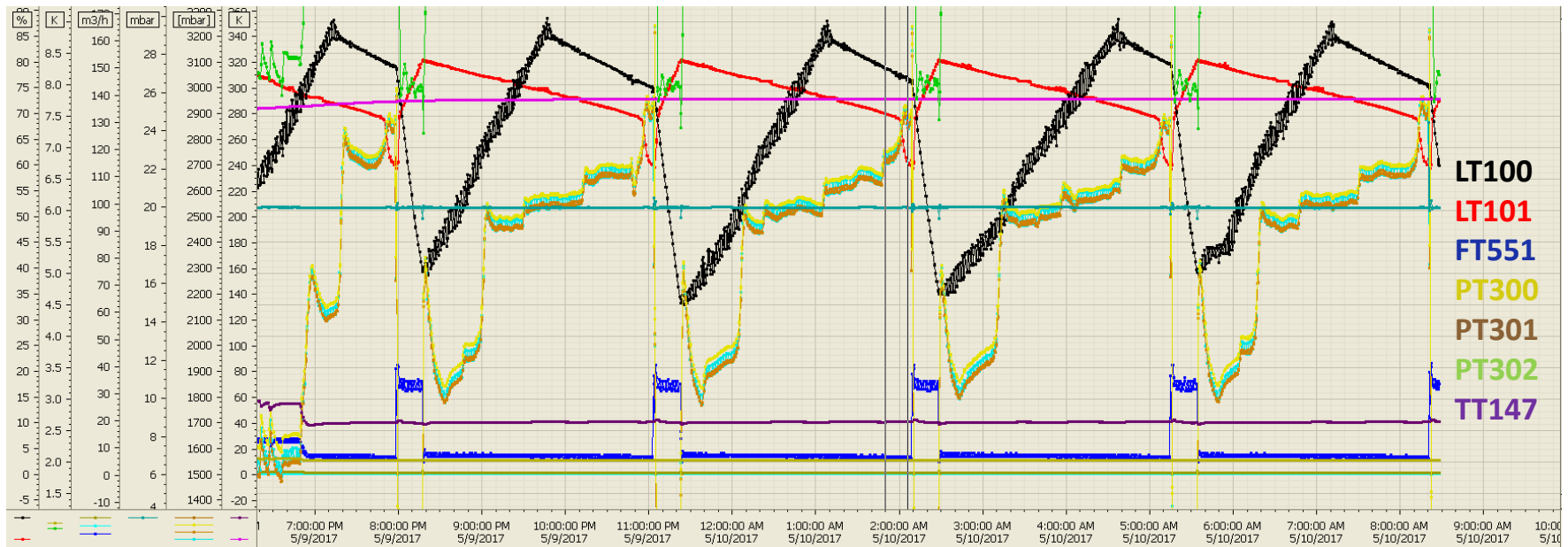


- The regulation of the valves CV301 and CV302 has to be fine-tuned: there are big variations in openings and thus in temperature while trying to regulate it to the set point.



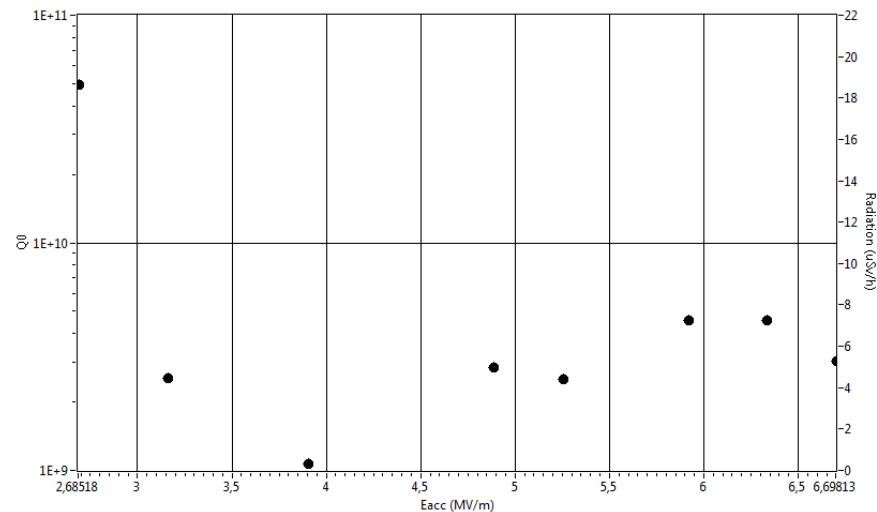
- Decided to regulate on constant flow instead. Kept it at 0.4 m<sup>3</sup>/h for coupler 2 and at a minimum of 0.8 m<sup>3</sup>/h for coupler 1 if no RF/heat power is applied.
- The maximum flow we have set coupler 1 to has been 1.2-1.4 m<sup>3</sup>/h, when going through either regions of high multipacting or when at high fields.
  - According to IPNO 0.4 m<sup>3</sup>/h for no RF power is already quite much, but it was the minimum to keep TT147 below 50 K. Are these values reasonable?
- In the future we will install an extra Cernox sensor at the interface between the cavity and the FPC since we had no idea how much heat the coupler (at T<sub>room</sub>) was bringing into the cavity. Also, This sensor might be better for regulating the temperature of the FPC instead of TT303.
  - According to the tests previously done measuring the effect of TT147 in FT551 (slide 11) as long as TT147 is kept below 90 K the extra heat load given is quite negligible. Still it seems counter intuitive to have such a mass at T<sub>room</sub> connected to 2K via thermalization at 40K (usually). Does this make sense?

- It was not possible to keep the pressure in the ScHe system constant: when the 2K tank fills the parameters in the ScHe system vary drastically and it takes quite some time for them to be back to normal. Also, when PT300 increases over 3.5 bar the SV to the recovery system opens, reducing the pressure.



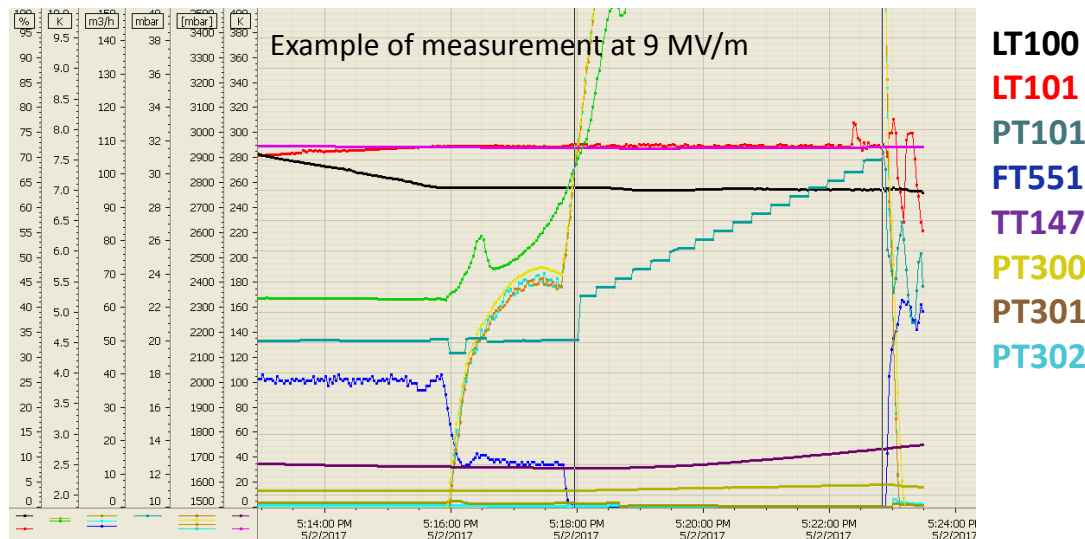
- How does the valves CV301 and CV302 regulate? When the system is being filled with GHe these valves reduce their opening and once the filling has stopped they open again to the given flow.

- The measurement for  $Q_0$  was done at 20 mbar and by keeping CV105 closed (no filling of the 2K tank) during measurements
- Two methods were used to calculate the  $Q_0$  slope:
  - By using the dynamic heat load given by FT551 (evaporation method)
  - By the pressure rise method
- **Evaporation method**
  - The level was kept between 73% and 77%
  - After the corresponding RF power was applied, the system was left to stabilise: stable pressure, stable flow and TT147 below 40 K (if possible)
  - The value given by FT551 at the time was used to calculate  $Q_0$



- **Pressure rise method**

- The level in the 2K tank was kept between 60% and 80%
- Initial calibration with varying heating power is done.
- After calibration, the desired RF power was applied and the system was left to stabilise only in pressure. This was because it took a long time to bring TT147 down and since TT147 had not so much effect on the flow when kept below 90K.
- Once the pressure was stable, the outlet valve CV552 would be closed and, after thirty (30) seconds, the RF team would measure the pressure rise for three (3) minutes.
- The first thirty seconds were never recorded because they showed a different slope. After ca. 30 s then the slope was constant . What is the reason behind for the change in slope?



- Measurement method for the pressure rise

➤ Calorimetric measurement of Q<sub>0</sub>

- ✓ close inlet and outlet valves of the cryomodule
- ✓ record the pressure as a function of time
- ✓ apply a known amount of resistive heat to the helium
- ✓ again record the pressure a function of time

Courtesy of H. Li

➤ Calorimetric measurement of Q<sub>0</sub> cont.

- ✓ build the calibration curve: the rate of pressure rise vs. heat
- ✓ load apply RF to the cavity, record the pressure rise
- ✓ calculate the dynamic RF load using the calibration curve

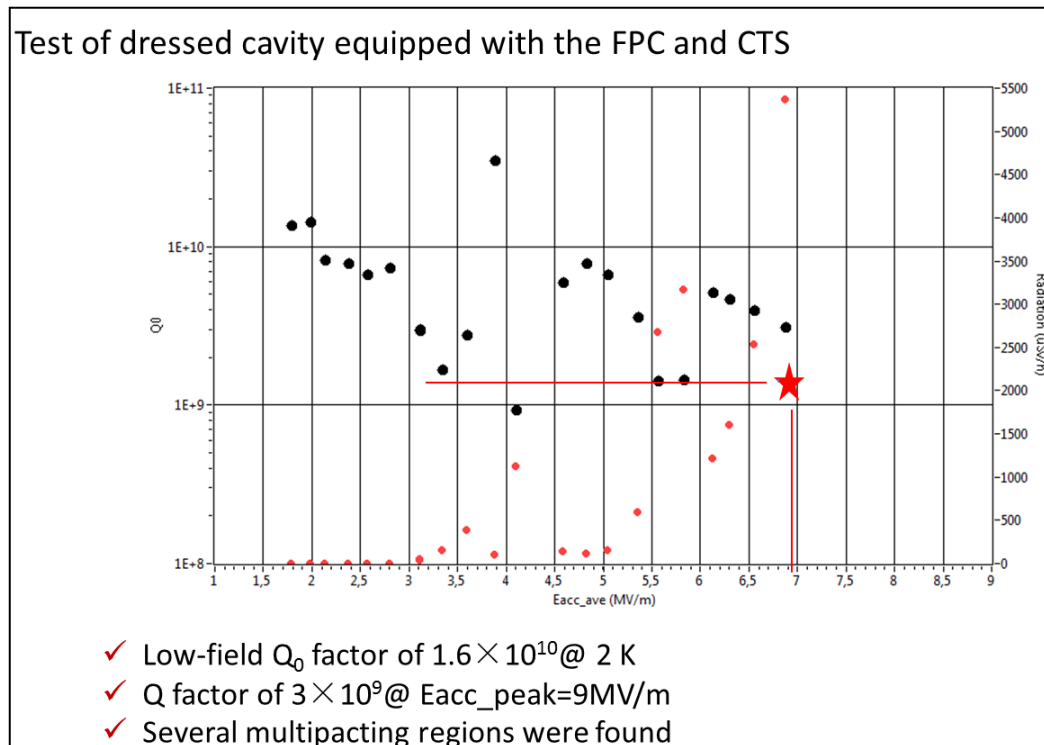
$P_m = m \cdot W + c$

$m = 0.0015 \pm 4.1520 \times 10^{-5}$   
 $c = 0.0155 \pm 3.2481 \times 10^{-4}$

Courtesy of H. Li

Static Heat load =  $0.0155 / 0.0015 = 10.3W$

- Q<sub>0</sub> slope obtained via pressure rise method



Courtesy of H. Li

- From these two different methods we get two different values for the static heat load of the cavity:
  - Evaporation method: 6 W – 7 W
  - Pressure rise method: 10 W
- How can we explain the difference?
  - The hydrostatic pressure at the top of the cavity would be  $P_{top} = P_{tank} + 6.5$  mbar and at the bottom  $P_{bottom} = P_{top} + 7.4$  mbar . To have a change from superfluid helium to normal helium the temperature must be 2.17 K (49 mbar), which would mean a maximum pressure of 35.1 mbar in the 2K tank. For some measurements, the pressure has not increased over 35 mbar and still we get a static heat load of 10 W...
  - During these measurements the ScHe circuit increases rapidly in pressure and TT1147 warms up, but remains below 90 K.

