Midterm presentation -Benchmarking a Cryogenic Code to the FREIA Liquefier

Elias Waagaard Supervisor: Volker Ziemann



UNIVERSITET

April 6th 2020





The FREIA He Liquefier





Background and project motivation

- Helium liquefier from Linde group
- Liquid He crucial for research infrastructure
- Simulations of thermodynamics better understanding of liquefaction process







Some thermodynamic concepts

Enthalpy

$$H=U+pV$$
, $U=U(T)$ for ideal gas

- Joule-Thomson (JT) valve
 - Irreversible, isenthalpic process: $\Delta H=0$
 - Inversion temperature
- Enthalpy in heat exchanger



$$H_2=H_1-dH \ H_4=H_3+dH$$





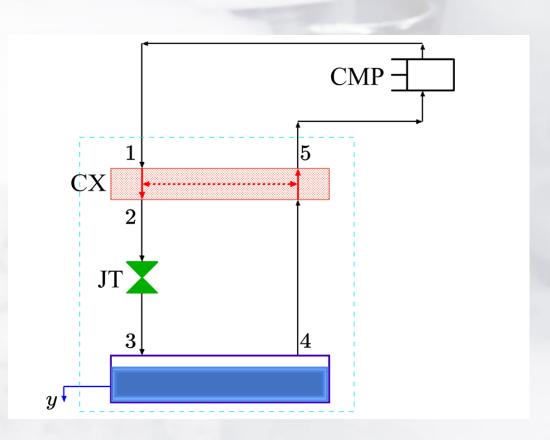
Liquefaction cycles - Linde

- Most fundamental cycle, 1895
- 1st law of thermodynamics in control volume (dashed):

$$\dot{m}h_1=\dot{m}_fh_f+(\dot{m}-\dot{m}_f)h_5 \ \Leftrightarrow \dot{m}h_2=\dot{m}_fh_f+(\dot{m}-\dot{m}_f)h_4$$

Yield:
$$y\equiv rac{\dot{m}_f}{\dot{m}}=rac{h_1-h_5}{h_f-h_5}$$

Local yield:
$$y_l \equiv \frac{\dot{m}_f}{\dot{m}_3} = \frac{h_2 - h_4}{h_f - h_4}$$





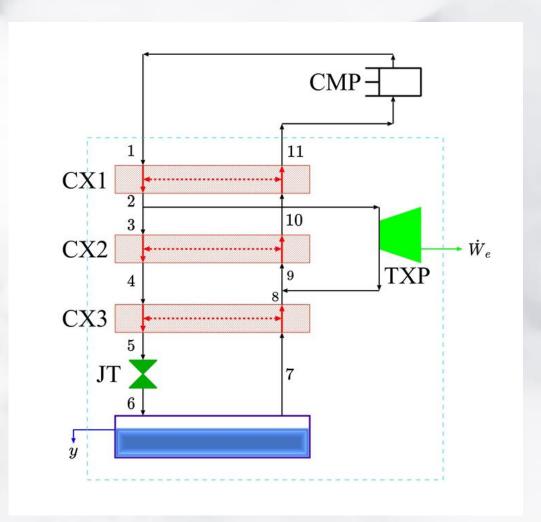


Liquefaction cycles - Claude

- Improvement, 1902
- Two more heat exchangers, isentropic expansion in turboexpander
- 1st law of thermodynamics:

$$egin{align} \dot{m}h_1 &= \dot{W}_e + (\dot{m} - \dot{m}_f)h_{11} + \dot{m}_f h_f \ & \ \dot{W}_e &= \dot{m}_e h_2 - \dot{m}_e h_e \ & \ x &= rac{\dot{m}_e}{\dot{m}} \ & \ \end{matrix}$$

$$y \equiv rac{\dot{m}_f}{\dot{m}} = rac{h_{11} - h_1}{h_{11} - h_f} + x rac{h_2 - h_e}{h_{11} - h_f}$$







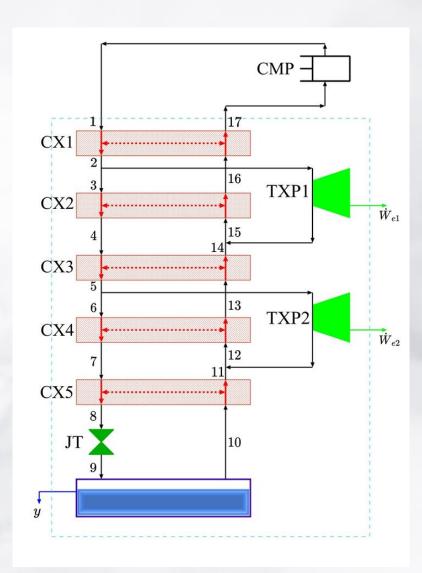
Liquefaction cycles - Collins

- Collins 1946
- Similar to Claude, but two more heat exchangers and one more turboexpander
- Analogously: 1st law around control volume gives

$$y \equiv rac{\dot{m}_f}{\dot{m}} = rac{h_{17} - h_1}{h_{17} - h_f} + x_1 rac{\Delta h_{e1}}{h_{17} - h_f} + x_2 rac{\Delta h_{e2}}{h_{17} - h_f}$$

with

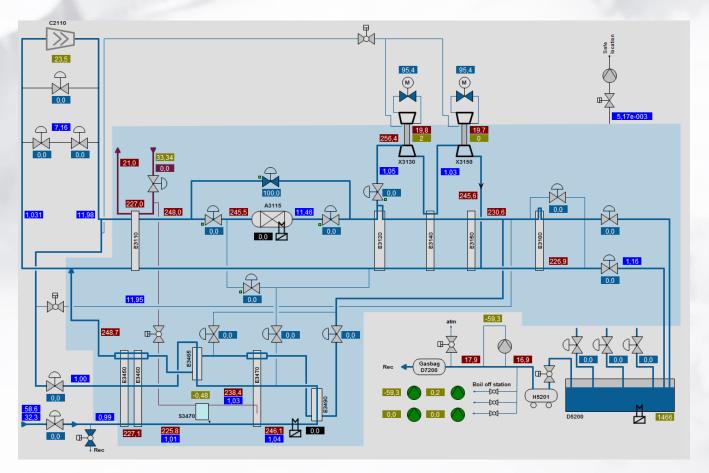
$$\dot{W}_{e_i}=\dot{m}_{e_i}\Delta h_{e_i} ~~x_i=rac{\dot{m}_{e_i}}{\dot{m}}$$
 , $i=1,2$



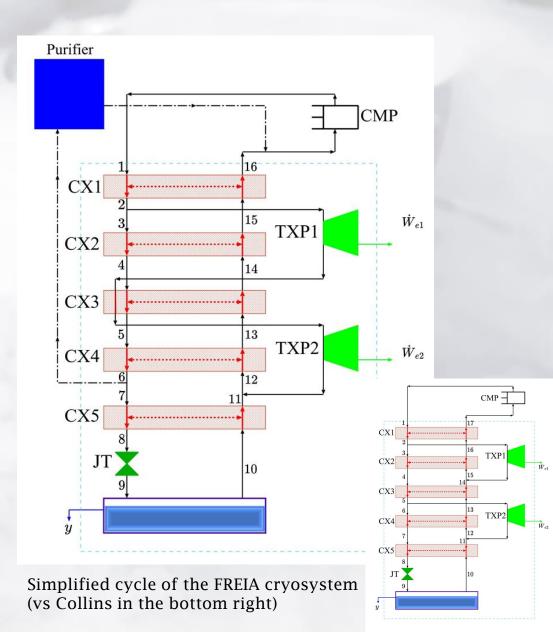




The FREIA System



The FREIA Liquefier Schematic with Coldbox







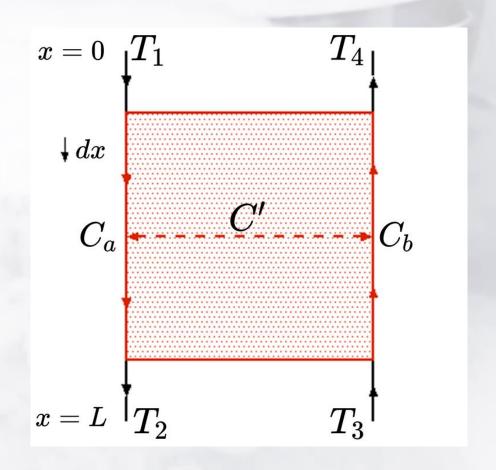
Cycle components: counterflow heat exchanger

System of linear equations

$$T_2 = T_1 - \eta (T_1 - T_3) \hspace{1cm} \eta = rac{1 - e^{-lpha}}{1 - rac{\dot{m_a}c_a}{\dot{m_b}c_b}} \eta (T_1 - T_3) \hspace{1cm} \eta = rac{1 - e^{-lpha}}{1 - rac{\dot{m_a}c_a}{m_bc_b}}$$

Enthalpy transfer

$$egin{align} \Delta \dot{H} &= C_H ig(T_3 - T_1ig) \ &C_H &= rac{C_a C_b (1 - e^{-lpha})}{C_a e^{-lpha} - C_b} & (C_a
eq C_b) \ &rac{1}{C_H} &= rac{1}{C_a} + rac{1}{C'L} & (C_a = C_b) \ \end{pmatrix}$$

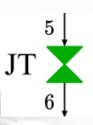




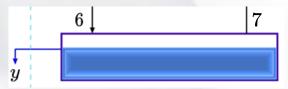


Cycle components - MatLab implementation

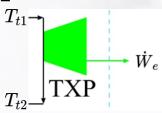
• JT valve:



Phase separator:



Turboexpander:



```
%JT-valve - isenthalpic process
T5= py.CoolProp.CoolProp.PropsSI('T','P',Phigh*le5,'H',H5/Q5,'Helium');
H6 = H5;
Q6 = Q5;
T6= py.CoolProp.CoolProp.PropsSI('T','P',Plow*le5,'H',H6/Q6,'Helium');
```

```
if T6 < 5.1953 %critical point of He
% enters liquid phase
hliq= py.CoolProp.CoolProp.PropsSI('H','T',T6,'Q',0,'Helium'); %specific heat capacity
hgas= py.CoolProp.CoolProp.PropsSI('H','T',T6,'Q',1,'Helium');
y1=(hgas-H5/Q5)/(hgas-hliq); y1=min(1,max(0,y1)); % local without HE
Hgas = H6 - y1*Q6*hliq;
H7= Hgas;</pre>
```

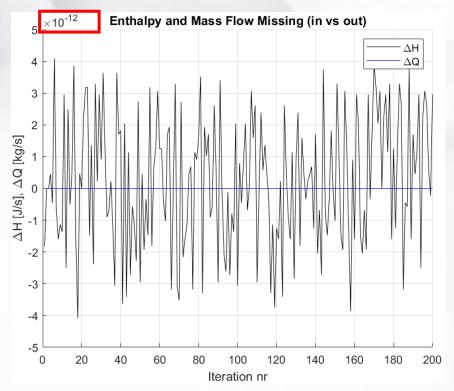
```
Ht1 = x*H2;
Tt1 = T2;
Tt2 = 0.5*T2;
Pt2 = Phigh/5.64;
ht2 = py.CoolProp.CoolProp.PropsSI('H','P',Pt2*1e5,'T',Tt2,'Helium');
Ht2 = x*Q1*ht2;
W = Ht1 - Ht2;
```

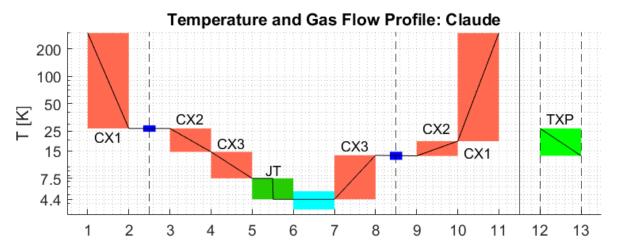


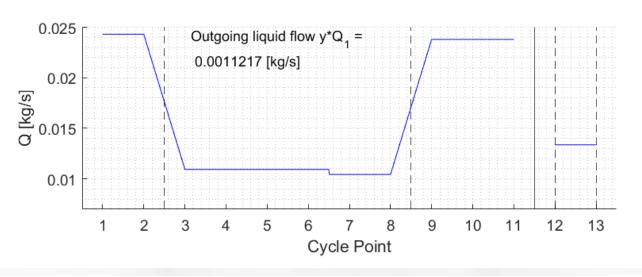


Simulations so far - Claude

- Iterative tester with MatLab function – convergence
- Enthalpy and mass flow conservation





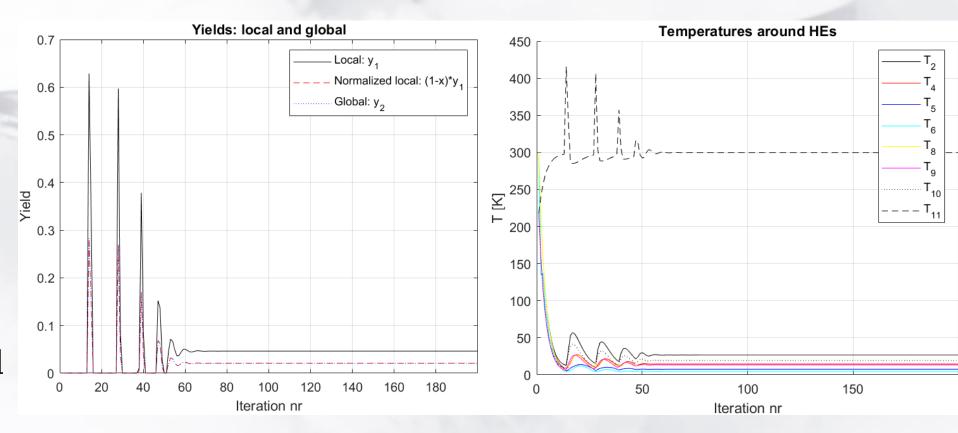






Next steps

- Oscillatory behaviour
- Convergence to low yields
- Implement the FREIA schematic
- Three-way heat exchanger
- Use actual T and P sensor values (if possible)







Thank you for your attention!

